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Errata as of September 26, 1999

Page	Correction
36	Figure $2-7 \rightarrow$ Figure 2-8
39	$expoxy \rightarrow epoxy$
51	$db \rightarrow dB$
59	"phono" \rightarrow phone
60	The term BNC is an acronym meaning "bayonet Neill Concelman". This connector is named after its designers, Paul Neill of Bell Labs and Carl Concelman of Amphenol. The "B" originally stood for "baby" but was changed to "bayonette" after the TNC connector was introduced to distinguish the bayonet fastening of the BNC connector from the threaded fastening of the TNC connector.
63	kilometer \rightarrow kilometers
83	Equation (3-7) should read $C_e = \frac{we}{s} + \frac{2\mathbf{pe}}{\log(4s/h)}$
85	Equations (3-10) is consistent if the current arrow is pointing to the left. However most people draw the current arrow pointing toward the right. In this case, both equations are negated becoming $\frac{\partial V}{\partial x} = -RI - L\frac{\partial I}{\partial t}$ $\frac{\partial I}{\partial x} = -GV - C\frac{\partial V}{\partial t}$
86	numerator \rightarrow middle term
93	delete ", the line"
94	$a \rightarrow a$ In three places, for example (a +1-V step). Here "a" is the word "a", not a symbol.
199	Equation (4-52) should read: $\frac{\partial I}{\partial V} = \mathbf{b} V_{GT} = \frac{2I_s}{V_{GT}} = g_m$
156	The equation in footnote 6 should read $V_{DE} = V_{DS} + V_{sat} - \left(V_{DS}^2 + V_{sat}^2\right)^{\frac{1}{2}}$
181	The last sentence should read: If the ratio of input capacitance to output capacitance $\eta=1.5,$
224	$Equation (5-2) should read:$ $V_{ji} = \frac{V_s Z_{ij}}{Z_0 + Z_{ij}}$ $Equation (5-3) should read:$ $V_R = V_s \left(1 - \frac{Z_{ij}}{Z_0 + Z_{ij}}\right)$
248	$10\text{mF} \rightarrow 10\text{-}\mu\text{F}$
264	As illustrated on the right side of Figure 6-2 \rightarrow As illustrated on the left side of Figure 6-2
267	Section $12.1 \rightarrow$ Section 12.2
269	$\mathbf{t}_{xp} \rightarrow \mathbf{t}_{xc in equations (6-5) and (6-6)}$

270	$\mathbf{t}_{xp} \rightarrow \mathbf{t}_{xc}$
	also:
272	Smear connecting the rightmost two conductors on Metal 3 in Figure 6-9 should be eliminated
213	Equation (0-9) should read $\frac{\partial V}{\partial t} (x, t) = \frac{\partial V}{\partial t} (x, t)$
	$\frac{\partial I_A(x,t)}{\partial t_A} = -\frac{\partial V_A(x,t)}{\Delta t_A}$
276	ot Lox
270	The correct values for κ_{cx} in Table 0-5 are:
	C
	These values represent $k_{cx} = \frac{C_m}{C}$ because C already includes C_m .
280	$ZP \rightarrow Z_P$
287	The second to last sentence should read
	If all this energy is absorbed by the silicon, which generates a hole-electron pair for each 3.6eV, then
	1.4M hole-electron pairs are generated, giving a total charge, $Q_{\alpha T}$, of 220fC.
289	Rather than use the absolute tolerances given in Table 6-4, most designers uses a statistical model of
	process variation based on [PelgDuin89]. With this model, variations are considered to have a
	normal distribution with a standard deviation that varies inversely to the square-root of the area of the device. That is
	$\frac{1}{2} \frac{1}{2} \frac{1}$
	$\Delta V_{Tn} = \frac{A_{VT}}{h_{TM}}$ and $\frac{\Delta D}{h} = \frac{A_{b}}{h_{TM}}$
	\sqrt{WL} D \sqrt{WL}
200	For a typical 0.55 mm process, $A_{VT} = 10 \text{mV}/\text{mm}$ and $A_b = 0.03/\text{mm}$.
290	
	$V_{IO} = \Delta V_{Tn} + 0.5 (V_{GS} - V_{Tn}) \left(\frac{\Delta D}{I} \right)$
295	$0.51 \rightarrow 0.48$
	also:
207	$1.02 \rightarrow 0.48$
297	$V_{\rm M}$ is the <i>net</i> noise margin, not the <i>gross</i> noise margin. gross \rightarrow net in two places.
307	$5.5 \text{IIIA} / 50 \text{S2} \rightarrow 5.5 \text{IIIA} \times 50 \text{S2}$
309	The bottom four numbers in the CMOS column of Table 7-3 should be: 2.05, 1.25, 1.25, 1.25
507	The bottom four numbers in the LSC column of Table 7-3 should be: 15, -15, 150, 150
310	The bottom row of Table 7-4 should be: 700, 18
	also:
	850mV, slightly more than half \rightarrow 700mV, almost half
	also:
211	$550 \text{mV} \rightarrow 400 \text{mV}$
311	In the first line: $50\% \rightarrow 25\%$
	also: $5./V \rightarrow 4./V$
	also: $92\text{mV} \rightarrow 72\text{mV}$
317	On the third line:
517	$I_{T_1} = V_{T_1}/Z_0 \rightarrow I_{T_1} = V_{T_1}/(Z_0 + Z_X)$
	also, equation (7-7) should be:
	$\left(\begin{array}{c} Z_{0} \end{array}\right) \left(\begin{array}{c} Z_{0} \end{array}\right)$
	$V_{X} = I_{X} Z_{0} = V_{T1} \left(\frac{Z_{0}}{Z_{0} + Z_{X}} \right) \left(\frac{Z_{RT}}{(N-1)Z_{RT} + R_{0} + Z_{0}} \right)$
	also, equation (7-8) should be:
	$K = \frac{(N-1)V_X}{(N-1)Z_{RT}} = \left(\frac{(N-1)Z_{RT}}{(N-1)Z_{RT}}\right) \left(\frac{Z_0}{(N-1)Z_{RT}}\right) < \frac{(N-1)Z_{RT}}{(N-1)Z_{RT}}$
	$V_{T1} = V_{T1} = (N-1)Z_{RT} + R_o + Z_0 \int Z_0 + Z_X \int^{-1} R_o + Z_0$

318	The lower part of Figure 7-7 should be labeled (b)
321	In Figure 7-11 (b) and (c), impedance Z_{RR} should be added between the bottom of R_T and the line
	return.
323	Note that in Figure 7-13, we have made the assumption that R_0 from Figure 7-4 is 0. Also, in
	Equations (7-11) and (7-12) we have assumed that $R_T = Z_0$.
325	Line series, termination \rightarrow line, series termination
	also:
	In 7.3.3.1 add:
	It should be pointed out that the major noise issue with source-terminated lines is that near-end cross
	talk appears at the far end of the line due to coupling of the reflected wave.
332	<i>The exponent in equation (7-23) should be negative.</i>
335	In Figure 7-28, the last pulse on V_R should be displaced one third of a bit cell to the right.
338	Substituting Eq. (7-28) into Eq. (7-29) \rightarrow Substituting Eq. (7-29) into Eq. (7-28)
	also:
	Equations $(7-31)$ and $(7-32)$ should have their denominators multiplied by LC
	also:
	in (7-32) $V(s) \rightarrow V_T(s)$
	Equation (7-34) should read
	$V_{\rm s}(t) = 1 - \exp\left(-\frac{Rt}{2}\right)\cos(wt)$
	$(2L)^{OOS(WV)}$
339	Equation (7-37) should read
	$t \to t \to t$
	$V_T(t) = U(t) - U(t - t_r) - \frac{t}{t}$
340	The negative ramp in Figure 7-33 should be labeled
	$-U(t-t_r)(t-t_r)/t_r$
341	$f \cong 2p \pm p/4 \rightarrow f \cong 2p \pm p/2$
342	<i>After</i> (7-46):
	$if \rightarrow If$
347	$K_{MN} \rightarrow K_{NM}$
348	Equation (7-62) should read:
	$V_L + K_h \Delta V$ if last bit was 0
	$U = \begin{cases} U = V_{II} - K_{I} \Delta V & \text{if last bit was } 1 \end{cases}$
240	
349	the slope of the transfer function must \rightarrow the slope of the transfer function, must
331	Jusi Dejore (7-00):
402	$uat \rightarrow so ulat$
405	The RMS value in Table 9-4 should be $\sqrt{\frac{1}{6}} = 0.408$
12.6	
450	In the first line, insert a comma (,) after the word 'stops'.
408	arives a current onto \rightarrow sinks a current off of
493	Replace a comma with a period after the sentence:
505	Lach state is labeled with the output (<i>ain, rout, go</i>).
510	Touring A Traing
542	$10 \text{uring} \rightarrow 1 \text{uring}$
343	In Figure 11-29, insert overbars over the right input of both amplifiers, <i>in</i> . Also insert an overbar
	over the left output of Figure 11-29 (b).
545	In Figure 11-31 there should be an overbar over the symbol ϕ driving the clock input of the clocked
	amplifier.
547	In Figure 11-33, insert overbars over the right <i>in</i> and the lower <i>s</i> .
649	$Bartovi \rightarrow Partovi$

659

659In the index entry for "impulse response" the page numbers should be: 545-547.Many thanks to Michael Werner at the Technion and Fred Rosenberger at Washington University for pointing out many of these mistakes.